



# Capturing carbon with chemical looping combustion of biomass

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# Content

Background and motivation

What is chemical looping combustion (CLC)?

What are negative CO<sub>2</sub> emissions?

Piloting of bio-CLC

Techno-economical assessment

Summary



## Background and motivation

What is chemical looping combustion (CLC)?

What are negative CO<sub>2</sub> emissions?

Piloting of bio-CLC

Techno-economical assessment, preliminary results

Summary



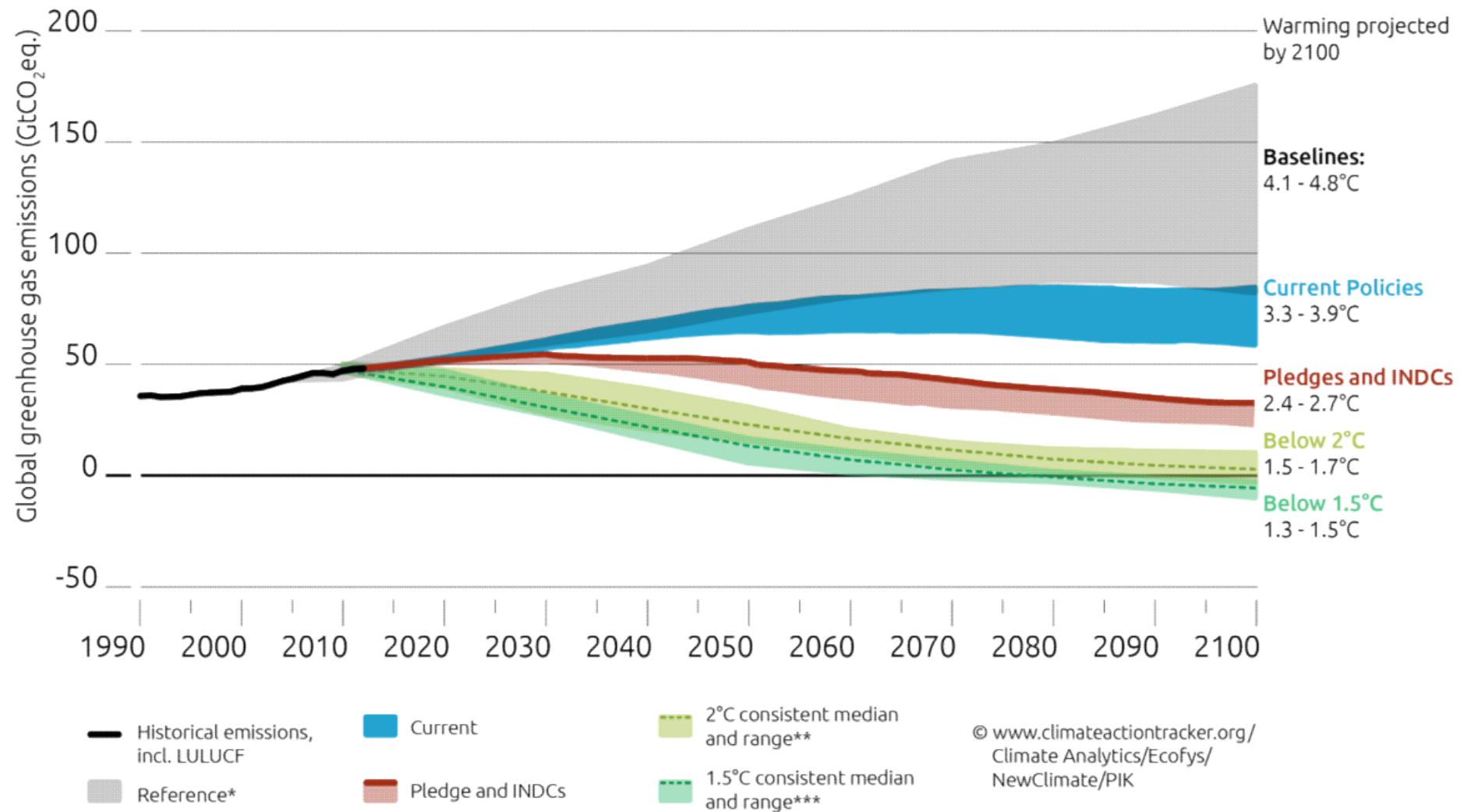
# After the Paris agreement the target is “CO<sub>2</sub> - neutral” society

- CO<sub>2</sub> removal technologies such as BECCS (Bio-Energy Carbon Capture and Storage) are becoming essential for achieving the 2 °C target <sup>1</sup>
- CCS and bioenergy as the two most valuable technologies for achieving climate policy objectives – more important than energy efficiency improvements, nuclear, solar power and wind power – motivated by their combined ability to produce very significant negative emissions via BECCS <sup>2</sup>

1. Climate Change 2014: Mitigation of Climate Change, Intergovernmental Panel on Climate Change, 2014.

2. Kriegler E., Weyant J., Blanford G., Krey V., Clarke L., Edmonds J., Fawcett A., Luderer G., Riahi K., Richels R., Rose S., Tavoni M., van Vuuren D, (2014), The role of technology for achieving climate policy objectives: Overview of the EMF 27 study on global technology and climate policy strategies, Climate Change 123, pp. 353-367.

# Negative GHG-emissions at end this century required to go below 2°C



- \* 5%-95% percentile of AR5 WGIII scenarios in concentration category 7, containing 64% of the baseline scenarios assessed by the IPCC
- \*\* Greater than 66% chance of staying within 2°C in 2100. Median and 10th to 90th percentile range. Pathway range excludes delayed action scenarios and any that deviate more than 5% from historic emissions in 2010.
- \*\*\* Greater than or equal to 50% chance of staying below 1.5°C in 2100. Median and 10th to 90th percentile range. Pathway range excludes delayed action scenarios and any that deviate more than 5% from historic emissions in 2010.

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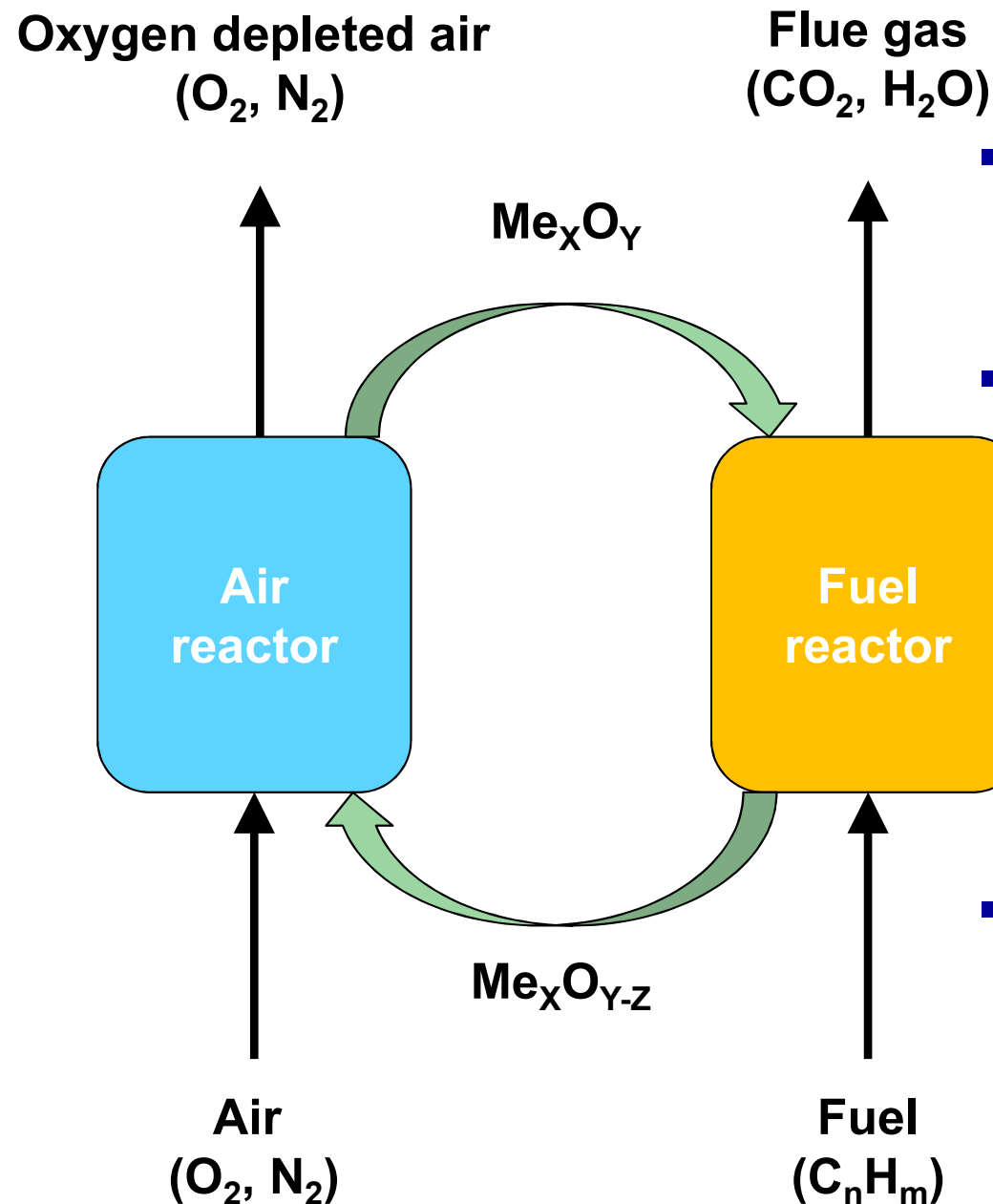
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# Chemical Looping Combustion – principle



- Oxygen carrier (OC):
  - transfers oxygen from air to fuel reactor
  - active part is metal (e.g. Fe, Cu, Mn, Ni, ...)
- Oxygen can be released
  - by heterogeneous combustion reaction between gaseous fuel and OC
  - by *in situ* gasification of solid fuel followed by heterogeneous combustion reaction (*iG-CLC*)
  - by chemical looping oxygen uncoupling (CLOU) where  $O_2$  is released due to effect of  $O_2$  partial pressure and temperature
- The total amount of released heat is the same as for normal combustion
  - Oxidation reaction in air reactor is highly exothermic
  - Reduction reaction is often endothermic

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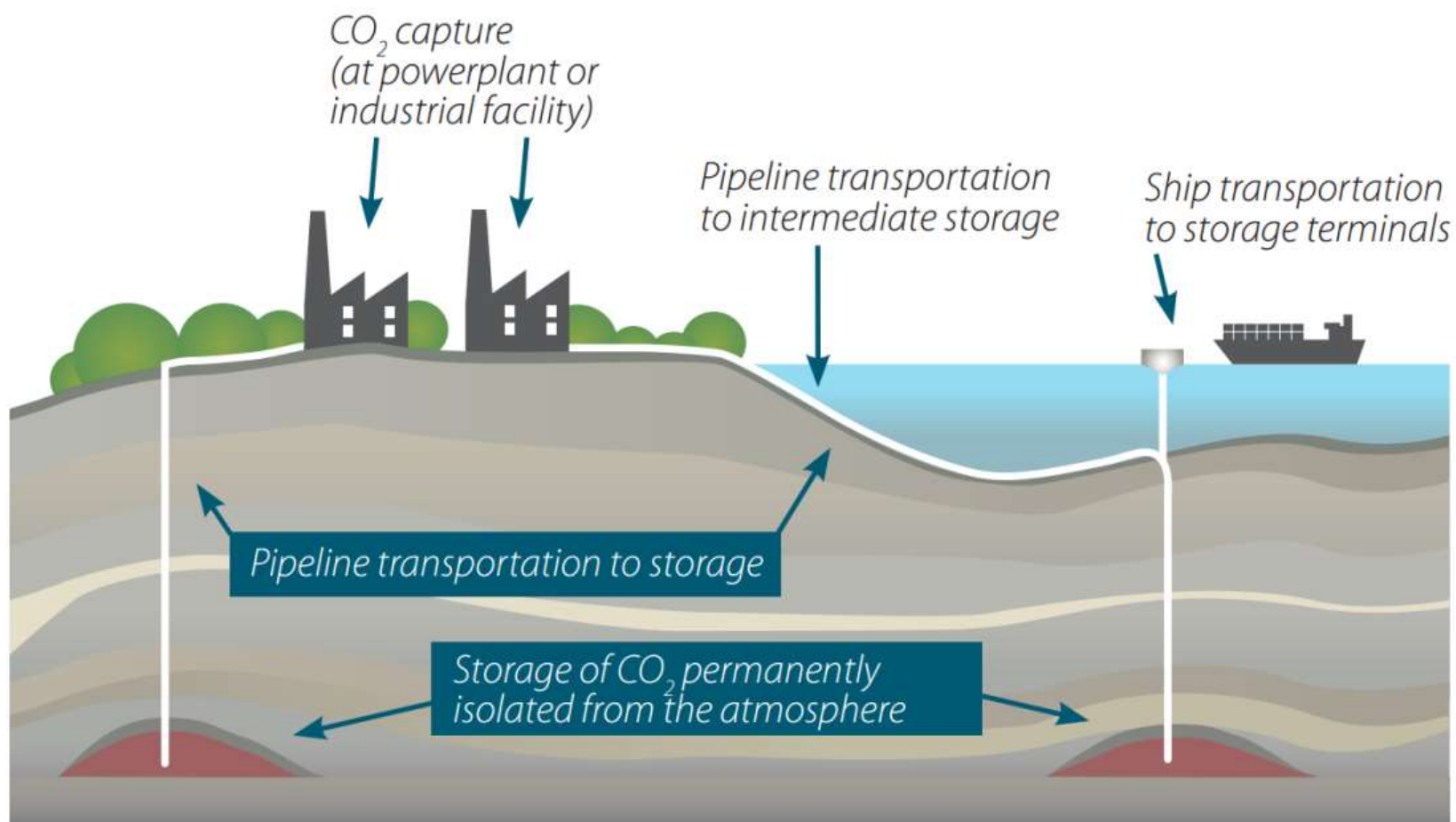
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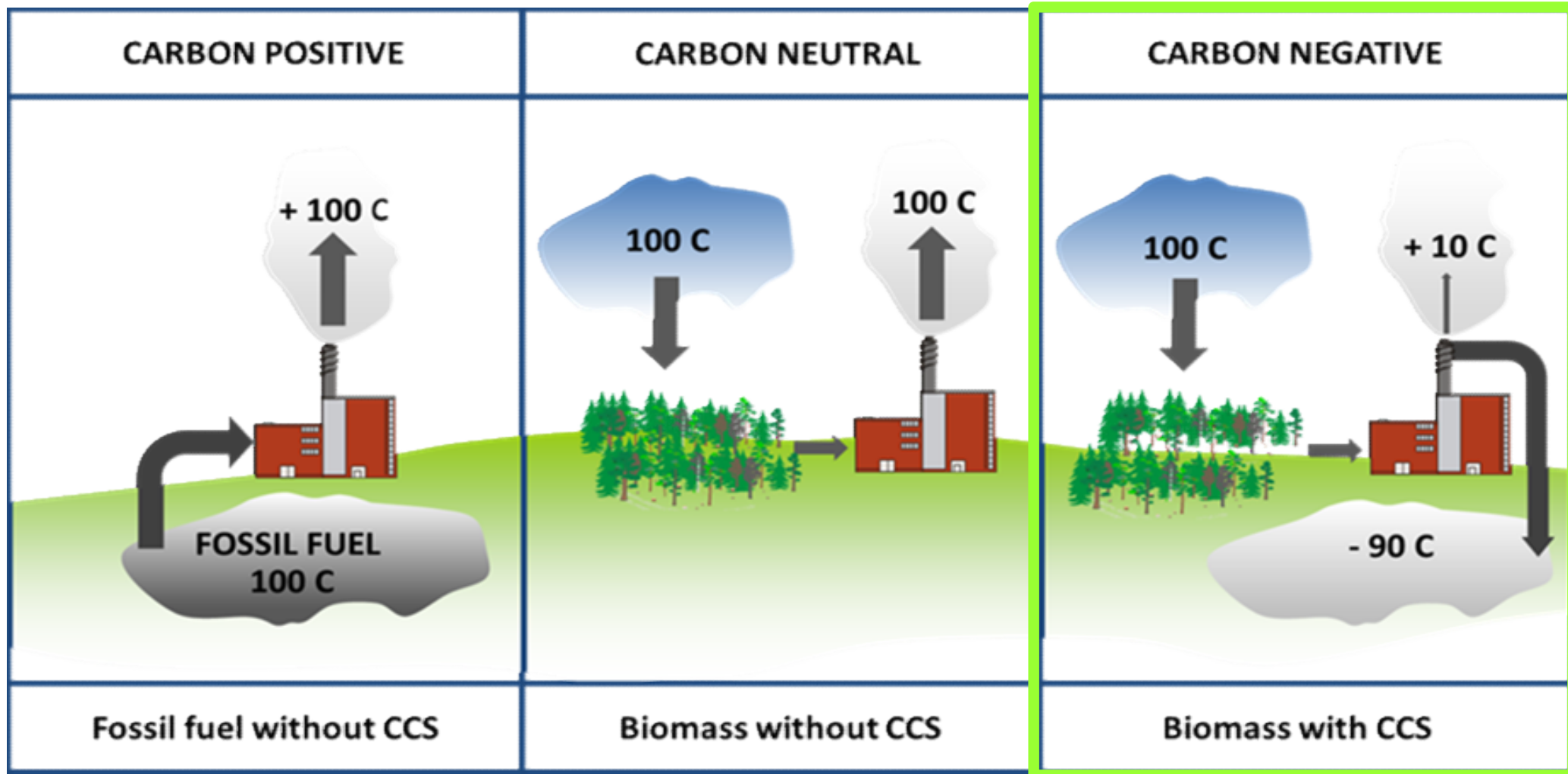
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# Carbon Capture and Storage - CCS



# Carbon balance



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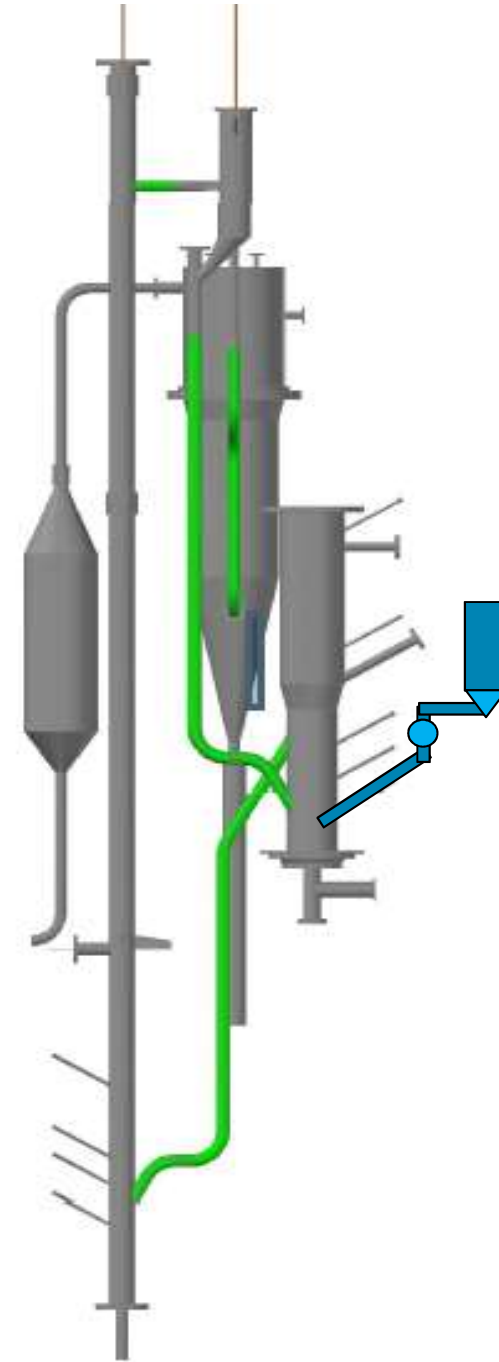
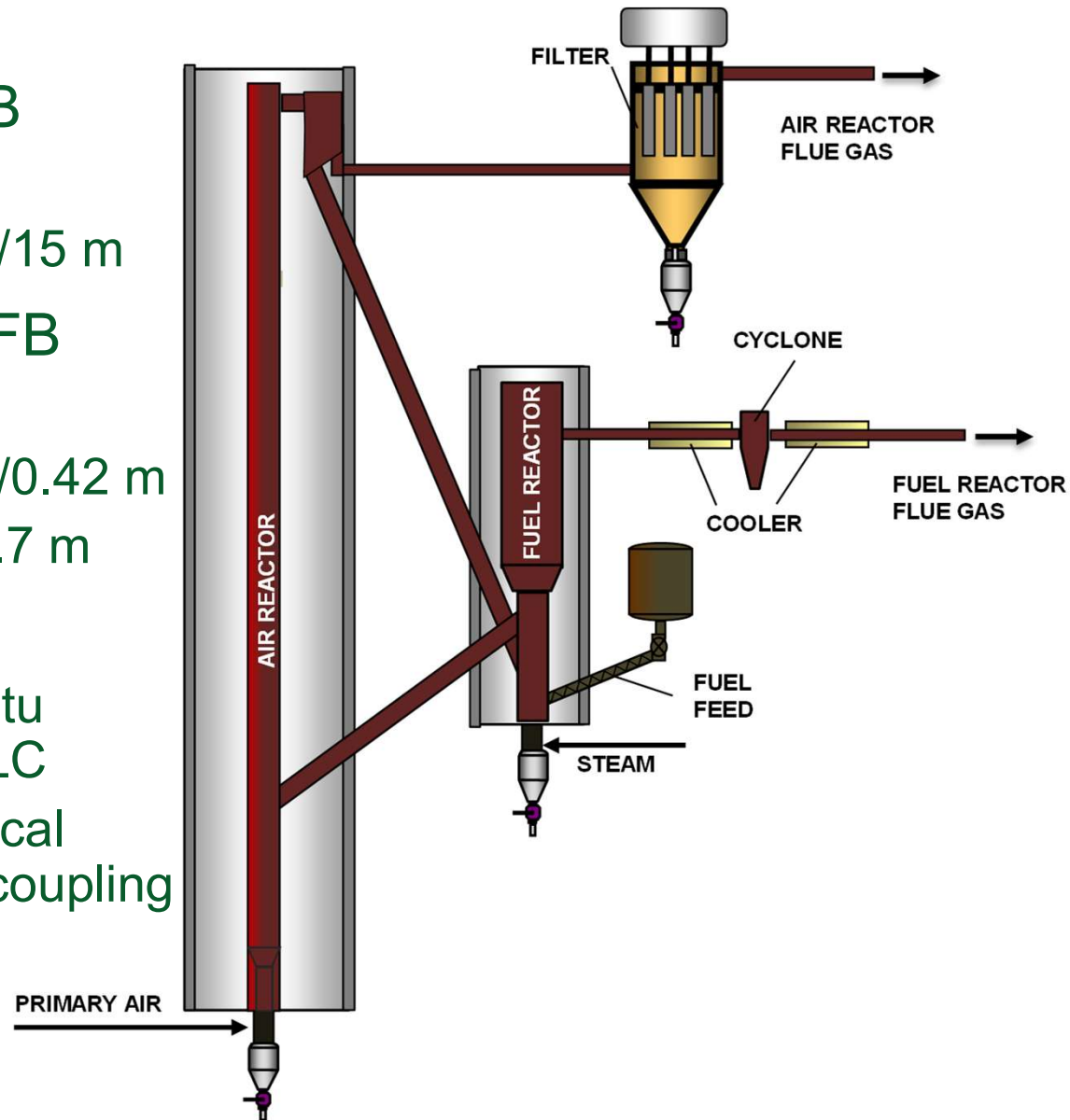
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# Dual fluidized bed CLC process development unit

- Air reactor - CFB
  - Height 8 m
  - Diameter 0.10/15 m
- Fuel reactor - BFB
  - Height 2.5 m
  - Diameter 0.32/0.42 m
  - Bed height ~0.7 m
- Fuel power
  - 10-20 kW in-situ gasification CLC
  - ~50 kW chemical looping  $O_2$  uncoupling



# Fuels and oxygen carrier



		VAPO white pellets	Arbaflame black pellets
Moisture	m-% a.r.	6.0	4.9
Ash	m-% a.r.	0.5	0.5
Volatiles	m-% a.r.	78.4	75.2
Fixed C	m-% a.r.	15.1	19.4
C	m-% a.r.	47.6	50.7
H	m-% a.r.	5.6	5.8
N	m-% a.r.	0.1	<0.1
S	m-% a.r.	<0.01	<0.01
O	m-% a.r.	40.2	38.1
LHV	MJ/kg a.r.	17.67	19.29

a.r. = as received


## Ilmenite (natural ore) oxygen carrier

- supplied by Titania A/S, Norway
- very pure (>95 m-%) ilmenite  $\text{TiFeO}_3$
- Narrow PSD,  $D_{50} = 270 \mu\text{m}$ ,  $D_{10} = 190 \mu\text{m}$  and  $D_{90} = 390 \mu\text{m}$
- bulk density of the fresh ilmenite  $2600 \text{ kg/m}^3$

# Test matrix and key performance indicators

High O<sub>2</sub> demand

But good C-capture



Test #	Fuel type	Duration min	Fuel reactor			Air reactor		Key indicators	
			Fuel kW	H <sub>2</sub> O m/s	Bed °C	Air m/s	Bed °C	Oxygen demand %	Carbon capture eff. %
1	VAPO white pellet	15	14	0.23	840	5.2	864	34	96
2		10	14	0.12	852	5.2	865	41	93
3		15	14	0.17	848	7.3	847	32	95
4	Arba-flame black pellet	20	15	0.23	845	5.2	869	32	94
5		10	15	0.12	863	5.2	875	38	92
6		25	22	0.17	848	6.0	878	34	88
7		20	19	0.17	852	7.4	868	30	83
8		40	9	0.12	860	7.4	862	29	86
9		15	19	0.12	851	6.5	872	31	87

- The main challenge encountered during the tests was to maintain a high enough bed temperature in the fuel reactor.
- The desired temperature level above 900°C, needed for optimal performance of the ilmenite oxygen carrier, was not achieved in any test.
  - As the DFB-PDU was originally constructed for gasification applications, its design is not optimal for chemical looping combustion.

# Conclusions from the pilot tests

- Promising results for using chemical looping combustion for biomass combustion with reduced risk of high temperature corrosion enabling the option to use higher steam values in bio-CLC than in conventional biomass combustion applications, improving the power generation efficiency.
  - This increase in efficiency could partially compensate for the efficiency loss due to the CO<sub>2</sub> compression or liquefaction needed for further transportation of CO<sub>2</sub> for final storage or use in chemical processes.
  - Although these results indicate a clear benefit of bio-CLC over conventional biomass combustion, this phenomenon needs to be studied in more detail for verification.
- Although the oxygen demand remained relatively high due to incomplete fuel conversion in the fuel reactor, the problem was mainly due to the PDU being originally designed for gasification.
  - Improvements planned (and use of CLOU materials as OC may help)
  - The problems are not expected to be an issue in a large scale application of bio-CLC.

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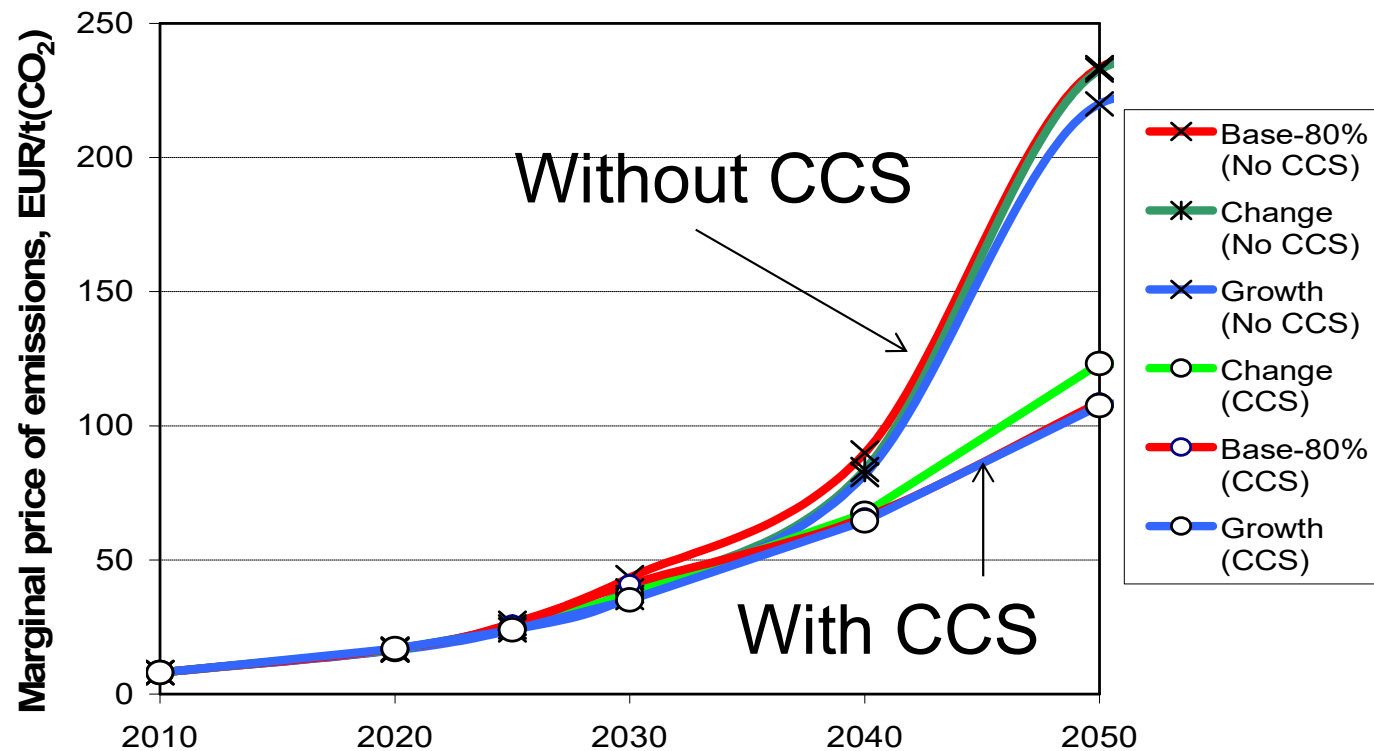
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## To study the role of CCS the CCSP scenarios were run with and without CCS

- In Base-80% scenario existing industrial and other economical structures result in higher CO<sub>2</sub> emissions
- In Growth scenario, CCS competes with rapidly developing other clean technologies
- In Change scenario only the bio-CCS is allowed. In addition the share of nuclear is the lowest.

CO<sub>2</sub> price doubles in those cases CCS is excluded



## Cost of carbon capture

Type of cost	estimation, €/tonne CO <sub>2</sub>	range, €/tonne CO <sub>2</sub>	Efficiency penalty, %
CO <sub>2</sub> compression	10	10	3
Oxy-polishing	6.5	4-9	0.5
Boiler cost	1	0.1-2.3	-
Oxygen carrier	2	1.3-4	-
Steam and hot CO <sub>2</sub> fluidization	0.8	0.8	0.8
Coal grinding	0.2	0.2	0.1
Lower air ratio	-0.5	-0.5	-0.5
Total	20	15.9-25.8	3.9

When applying  
OTSC steam cycle  
10-15% efficiency  
improvement  
potential  
(~3.5-5.5 %-p.)

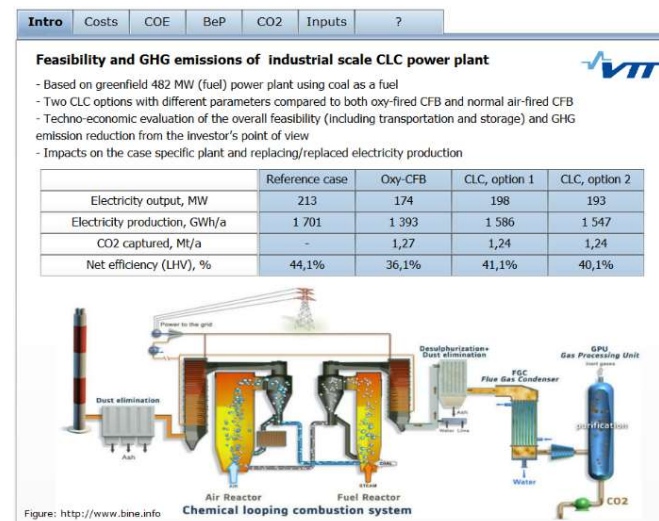
*Taken from: Lyngfelt, A.; Leckner, B., "A 1000MWth boiler for chemical-looping combustion of solid fuels-Discussion of design and costs", Applied Energy, 2014, In press.*

# Techno-Economic Assessments of CLC concepts

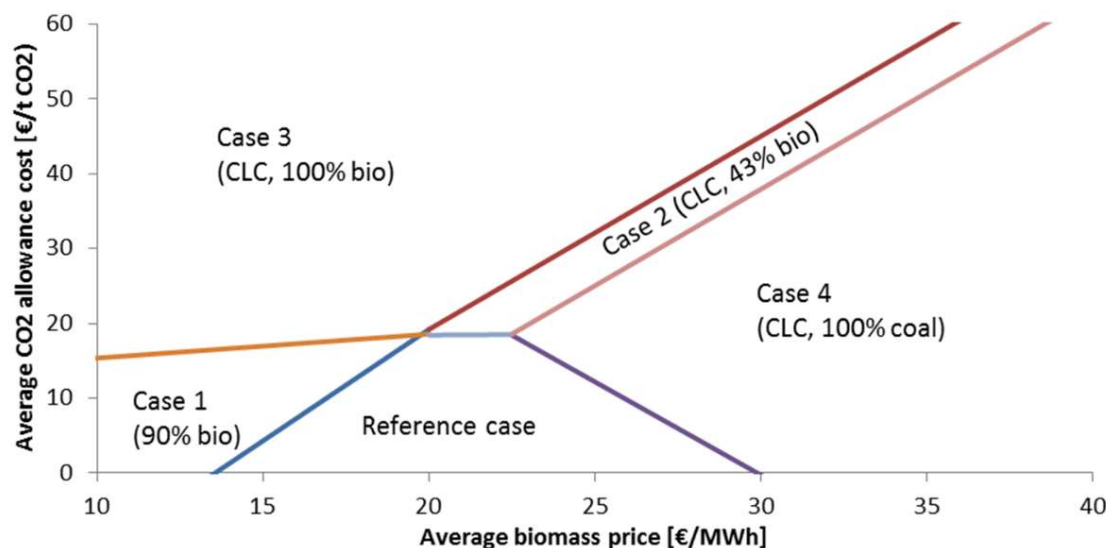
## Several case studies conducted:

- Prefeasibility-type-of assessments
- Profitability of CLC plant investment and operation in different market conditions
- CHP and condensing plants at commercial scale (up to 500 MW<sub>fuel</sub>)
- Comparison to oxy- and air-fired CFB
- Biomass, coal, natural gas, co-firing

- Costs of captured CO<sub>2</sub> as low as 20 €/t



See TEA example on-line: [Techno-economic toolkit](#)



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- Negative GHG-emissions at end this century required to go below 2°C
- Bio-CCS only industrial scale carbon negative technology that can be deployed today
- Chemical looping combustion is a novel technology enabling CCS with lower energy penalty compared to other CCS technologies
- Promising experimental results of bio-CLC with reduced risk of high temperature corrosion enabling the option to use higher steam values in bio-CLC than in conventional biomass combustion applications, improving the power generation efficiency.
- Techno-economical assessments show superior performance of CLC/bio-CLC

➤ Next step: demonstration in industrial scale

# Acknowledgements

- This work was carried out in
  1. The Carbon Capture and Storage Program (CCSP) research program coordinated by CLIC Innovation Oy with funding from Tekes - the Finnish Funding Agency for Innovation
  2. The Nordic Flagship Project No: 77732 “Negative CO<sub>2</sub> emissions in the Nordic energy system” (2015-2019) funded by Nordic Energy Research





**Thank you!**  
**Questions?**

## Back-up slides

# Corrosion risk in air reactor flue gas path

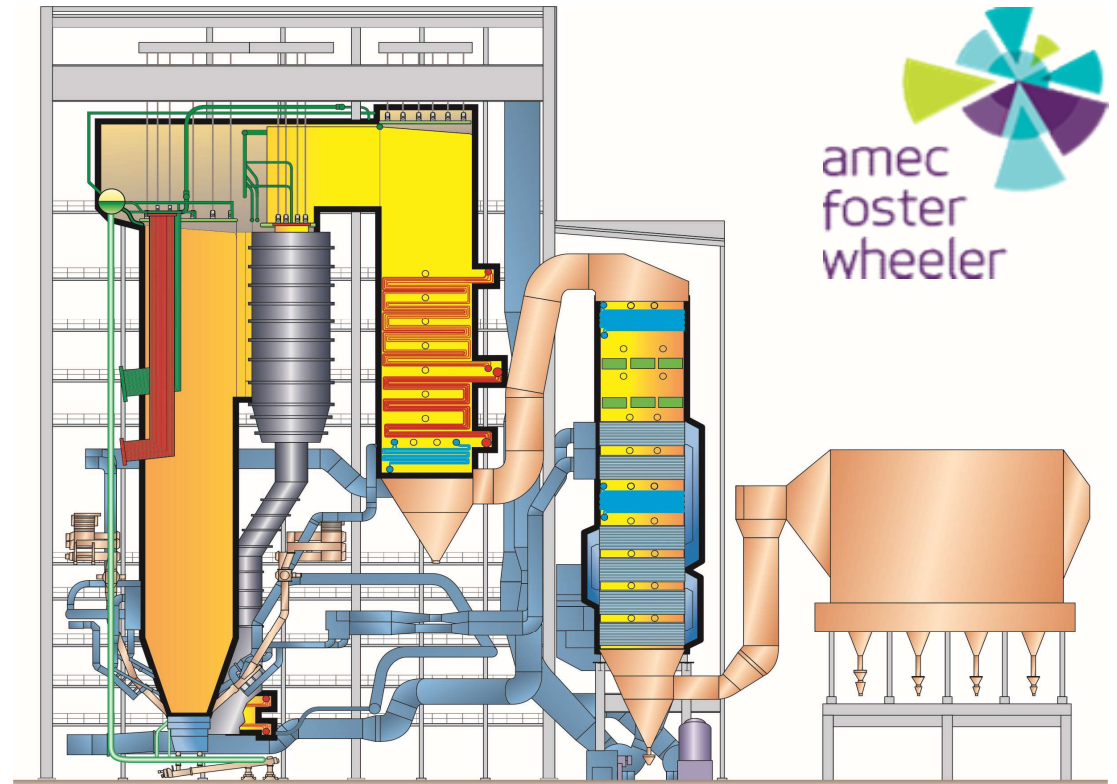


- The CO<sub>2</sub> concentration in the air reactor flue gas was <0.2 vol-% (dry) indicating insignificant combustion reactions.
- No indications of accumulation of alkaline components to the surface of oxygen carrier particles were found according to XRF analyses
- No alkaline containing aerosols found from the gas flow sampled before the filter (at ~450°C)
- Chlorine concentrations were under the detection limit in all samples.
- It can be concluded that concentrations of vaporized alkali chlorides components in air reactor flue gas are much lower than in conventional biomass combustion applications.
  - This reduces the risk of high temperature corrosion of super heater tubes enabling the option to use higher steam values (temperature, pressure) improving the power generation efficiency.
- Although these results indicate a clear benefit of bio-CLC over conventional biomass combustion, this phenomenon needs to be studied in more detail for verification.

- *Bio-CLC could be profitable also without CCS.*
  - It is expected that high-temperature corrosion problems can be significantly reduced in Bio-CLC as compared to conventional biomass combustion.
  - This is because heat will be extracted mainly in the exothermic air reactor, in which there will be no alkali compounds present and very little fly ash.
  - This should allow the use of improved steam data compared to conventional biomass combustion and improved efficiency for power generation.
  - Hence implementation of Bio-CLC could in fact be economically feasible already before there is an infrastructure for CO<sub>2</sub> transport and storage available.
- *Bio-CLC could be demonstrated in large scale at lower economic risk.*
  - A demonstration plant could be designed so that it would be possible to operate it also as an ordinary CFB boiler.
  - This means that after the demonstration period, the unit could be operated in CFB mode if its performance in CLC mode is unsatisfactory.
  - This would reduce the economic risk of such a venture greatly, if there is need for a utility on the demonstration site.

# World's Largest CFB Firing 100 % Biomass

Polaniec, Poland, 569 t/h, 447 MW<sub>th</sub>



- Customer: GDF Suez Energia Polska
- Plant start-up: Q4, 2012
- Fuels: Wood biomass + max 20 % high-alkaline agro biomass
- Design features:
  - CFB furnace 24 m x 7.6 m x 43 m
  - Three steam-cooled separators
  - Step grid
  - Additive feeding systems
  - INTREX SH 3 & RH 2

<b>Electrical output, gross/net</b>	<b>MW<sub>e</sub></b>	<b>205/190</b>
<b>Net efficiency, LHV/HHV</b>	<b>%</b>	<b>36.5/31.4</b>
<b>Steam flow rate, SH/RH</b>	<b>kg/s</b>	<b>158/135</b>
<b>Steam pressure, SH/RH</b>	<b>bar, g</b>	<b>126/19</b>
<b>Steam temperature, SH/RH</b>	<b>°C</b>	<b>535/535</b>

<b>Emission</b>		<b>Guarantee</b>	<b>Measured<sup>(1)</sup></b>
<b>NO<sub>x</sub></b>	<b>mg/m<sup>3</sup>n</b>	<b>150</b>	<b>140</b>
<b>SO<sub>2</sub></b>	<b>mg/m<sup>3</sup>n</b>	<b>150</b>	<b>3</b>
<b>CO</b>	<b>mg/m<sup>3</sup>n</b>	<b>50</b>	<b>&lt; 5</b>
<b>Dust</b>	<b>mg/m<sup>3</sup>n</b>	<b>20</b>	<b>4</b>

1) F. van Dijen, H. Gennart, "The New 200MWe Wood-Fired CFBC at Polaniec/Poland"